

Optimization of operational parameters at laboratory scale membrane bioreactor for treatment of high-strength opium alkaloid wastewater: The effect of pretreatment

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Abstract

Two different membrane treatment scenarios have been applied for treatment of the high strength dark color alkaloid industry wastewater. A membrane bioreactor (MBR) system having separately UF and MF membranes was operated with raw alkaloid wastewater treatment (scenario-A) and anaerobically pre-treated alkaloid wastewater (scenario-B). NF 270, NF 90 and RO (XLE) membranes were used as a polish-ing step at two different recovery ratios of 50% and 75% for both scenarios. In scenario-A, the COD re-moval efficiencies for MBR-MF and MBR-UF were found as 86±9% and 55±24%, respectively. At the polishing step, RO performance after scenario-A indicated that the 99.6% COD and complete color remov-al was achieved. On the other hand, in the scenario-B, the COD removal efficiencies for MBR-MF and MBR-UF were found as 41±16.4% and 24±18.3%, respectively. RO experiments with raw wastewater indi-cated that the 99.6% COD and complete color removal were achieved. The most crucial problem during direct MBR operation was found as a foaming problem and prevented by anti-foaming agent which caused an increase in effluent COD concentration and chemical cost. For these reasons, it can be concluded that MBR operation with anaerobically pre-treated was more effective than the other scenario.

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1. Introduction

The opiate is a chemical naturally existing in the opium poppy plant, and it is consumed on a big scale by medical sectors and scientific areas. The significant alkaloids are classified as morphine, codeine, thebaine, narcotine, and papaverine [1]. During the production process, the poppy capsules are ground and treated with lime, and the slurry is pressed to extract the liquid that contains the alkaloids. The liquid's pH is adjusted by adding Na₂CO₃ and a filtration process separates the impurities. In the extraction process, the alkaloids are extracted with specific solvents such as toluene and butanol. The morphine is crystallized by adding NH₄OH and separated from the solution by centrifuges. The used solvents and the water are sent to the distillation column to recover toluene, alcohol groups and the remaining wastewater treated in wastewater treatment plant [2]. The opium is cultivated and processed in a few countries such as India,

Australia, France, Hungary, Spain, Ukraine, Yugoslavia, and Turkey [3]. However, a limited number of researchers have worked on the treatment of alkaloid wastewater until now. Biological and physicochemical treatment studies on the effluent of opium wastewater treatment plant were performed by Kınlı [4], and chemical oxygen demand (COD) removal efficiency reached 70% in anaerobic treatment process. Also, ozone oxidation was used as the pretreatment technology of the aerobically treated effluents, and the color and COD removal efficiencies of the process were found at 87% and 30%, respectively. Ozturk et al. [5] also investigated the anaerobic treatment for composite wastewater generated from the process water (extracting from distillation column section) and domestic wastewater of an alkaloid industry. In this study, a full scale Anaerobic Internal Cycling (AIC) reactor was operated with an organic loading rate (OLR) of 5 kg

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COD/m³.day. COD and VFA removal efficiencies were found as 85 and 95%, respectively. The biogas production rate was obtained as 0,1-0,35 m³ CH₄/COD_{removed}. The main operational parameters stated in the study were very high salinity and sulphate concentration in composite wastewater. Sakar et al. [6] operated an electro dialysis (EC) process for sulphate removal from the concentrate stream at nanofiltration (NF) membrane process of alkaloid wastewater. They concluded that 99% of sulfate concentration was retained by membrane and found in concentrate streams of NF90 and NF245 membranes.

Aytimur and Atalay [7] worked on reducing the organic matter in Alkaloid Industry raw wastewater and operated a conventional activated sludge system for biological treatment with 88% COD removal and also the catalytic wet air oxidation (WAO) process for extra chemical oxidation with the COD removal efficiency of 35%. They concluded that combining these processes is not very effective, and the biological treatment was sufficient for reaching high COD removal efficiency as a single process. Similarly, Kacar et al. [8] investigated the pretreatment of the alkaloid processing wastewater in Turkey by WAO followed by the pressure and temperature on COD removal. The catalyst types in the experiments were Cu(NO₃)₂, Co(NO₃)₂, Ni(NO₃)₂, FeCl₂. They reported that above 26% of COD removal efficiency was obtained in 2 h of operating time at 150 °C, 0.65 MPa, and an airflow rate of 1.57 x 10⁻⁵ m³s⁻¹. Bural et al. [9] investigated the effect of gamma irradiation as pretreatment step on aerobic biological treatment of opium alkaloid wastewater. Two sequencing batch reactors (SBRs) were used as a biological treatment setup in the experiments, one of the reactors was fed with raw wastewater without any irradiation, and the other one was operated with irradiation of 40 kGy at the same raw wastewater. The reactors were gradually fed with increasing COD concentrations because of biomass acclimatization to opium alkaloid wastewater. At the operation with 5000 mg/L COD concentration, the COD removal efficiencies were 79% and 73% for reactors fed with raw and irradiated wastewater, respectively.

Another anaerobic treatment study of alkaloid processing wastewater was presented by Aydin et al. [10]. The treatment study was conducted at an 11.5 L lab-scale UASB (Upflow Anaerobic Sludge Bed) reactor for 825 days under different hydraulic retention times (HRTs) (0.84-1.62 days) and organic loading rates (OLRs) (3.4-12.25 kg COD/m³day) at 35±2 °C. The COD removal efficiency slightly decreased with the increase of OLR and decreasing HRT. However, the UASB reactor was operated at high COD removal

efficiency varying between 74-88%. They also identified some toxic organic chemicals such as N, N-dimethylaniline, and toluene in the opium wastewaters. These compounds are known to be inhibitory for biological treatment processes. Dereli et al. [11] applied Anaerobic Digestion Model No. 1 (ADM1), developed by the IWA (International Water Association) Task group for Mathematical Modeling on Anaerobic Digestion, for the data obtained by Aydin et al. [10]. The validation results indicated that the calibrated ADM1 could predict the experimental results of effluent COD and pH with reasonable accuracy, whereas some discrepancies were observed for methane gas productions. Cengiz et al [1] worked on the hydrothermal gasification of opium alkaloid wastewater and found 95% COD removal efficiency at 600 °C in the presence of a catalyst at an amount of 0.375–0.625 g. Koyuncu [12] carried out membrane treatability studies, and Koyuncu et al. [13] carried out the membrane process and ozonation experiments on the opium alkaloid industry. Lab-scale membrane and ozonation reactors were performed in the experiments. Low-pressure reverse osmosis membranes were used to remove COD, color, and conductivity from biologically pretreated opium alkaloid industry effluents. The influent COD, color, and conductivity were measured as 1900 mg/L, 1750 Pt-Co, and 3500 µS/cm. The removal efficiency of COD, color, and conductivity were found greater than %99. Moreover, they experienced 41% of COD treatment efficiency with ozonation applied in biologically treated opium alkaloid wastewater in 50 min. The dark-red brownish color of wastewater turned to light yellow after 50 min. of ozonation with 96% of color removal efficiency. Gencsoy [14] investigated the anaerobic treatment of the opium alkaloid industry. A laboratory scale UASBR was operated at different organic loading rates varying from 3.75 to 10 kg COD/ m³-day at mesophilic conditions. It was found that anaerobic treatment's COD removal efficiency reached 87% at UASBR for 5 kg COD/m³-day organic loading rate. Besides, the ratio of CH₄ content in produced biogas was measured as 72%. From all literature studies, it is concluded that the anaerobic pre-treatment is a very feasible process to upgrade the existing full-scale activated sludge system for the industry.

This study aims to apply two different scenarios to treat the opium alkaloid processing industrial wastewater. The first scenario was the direct application of membrane bioreactor (MBR) for raw alkaloid wastewater treatment without any pretreatment process. At the second scenario, the MBR system was operated after anaerobically pretreated alkaloid wastewater. The polishing step was applied for both

scenarios using NF and RO membranes. The study's primary purpose is to investigate the effect and importance of the anaerobic pretreatment of high-strength opium alkaloid wastewater before the application of membrane technologies and to compare the results of two scenarios. Opium alkaloid wastewater is very complex wastewater and has high pollutant concentrations. For this reason, different membrane treatment scenarios were proposed in this study to solve this significant industrial wastewater pollution problem. The study's novelty is to evaluate the different operating scenarios with and without

pretreatment and build an optimum and sustainable treatment process flow-chart.

2. Material and Methods

2.1. Wastewater characteristics

The raw wastewater was taken from the opium alkaloid processing plant which located in Afyon Province in Turkey. The characteristics of raw wastewater and the discharge standards of receiving environment at the effluent stream of the wastewater treatment plant are shown in Table 1. All analyses were carried out according to Standard Methods [15].

Table 1. Characteristics of wastewater streams used in the experimental runs

| Parameters | Properties of raw wastewater | Discharge standards ^a |
|--|------------------------------|----------------------------------|
| pH | 4.7±0.6 | 6-12 |
| Biochemical Oxygen Demand (BOD) (mg/L) | 10151±3908 | - |
| Chemical Oxygen Demand (COD) (mg/L) (as soluble) | 32995.±8811 | - |
| Total Suspended Solid (SS) (mg/L) | 427.5±235 | - |
| Volatile Suspended Solids (VSS) (mg/L) | 426±217.5 | - |
| Total Dissolved Solids (TDS) (mg/L) | 41133±6559 | 500 |
| Inorganic TDS (mg/L) | 15910±8584 | - |
| Conductivity (µs/cm) | 29750±10111 | - |
| Volatile fatty acids (VFA) (mg/L) | 5806±1773 | - |
| Total Kjeldahl Nitrogen (TKN) (mg/L) | 561±71 | 15 |
| Ammonium Nitrogen (NH ₄ -N) (mg/L) | 22±5.6 | - |
| SO ₄ ²⁻ (mg/L) | 11656±4087 | 1700 |
| Total Phosphorus (TP) (mg/L) | 23.8±6.7 | - |
| Alkalinity (mg/L CaCO ₃) | 4504±1866 | - |
| Color (Pt-Co) | 2500 | - |
| Particle size, µm | 13.18 | - |

^a Water Pollution Control Regulations of Turkey

2.2. Properties of membranes

Nanofiltration (NF) and reverse osmosis (RO) membranes were provided by Dow/Filmtec and the

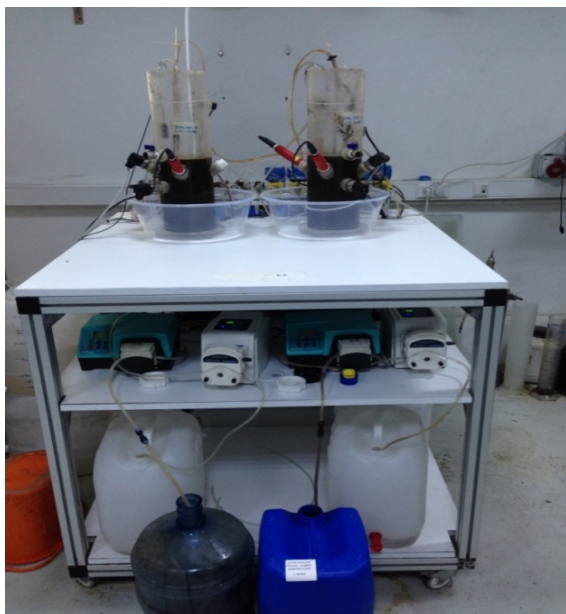
microfiltration membrane (MF) was purchased from Microdyn Nadir. Table 2 provides some information of the membranes given by the manufacturers.

Table 2. The technical characteristics of used membranes

| Membrane | Manufacturer | Molecular weight cut-off, (Da) / Pore size (μm) | Material | Flux ($\text{L}/\text{m}^2\cdot\text{h}$) |
|----------|----------------|--|------------------|---|
| MP 005 | Microdyn Nadir | -/0.05 | Polyethersulfone | > 200 |
| NF 270 | Dow | ~200-400/- | Polyamide | 42-58 |
| NF 90 | Dow | ~200-400/- | Polyamide | 27-35 |
| XLE | Dow | ~100 /- | Polyamide | 19-24 |

2.3. Experimental set-up

This study examined the treatment of high-strength dark color opium alkaloid processing industry wastewater and anaerobically pretreated opium alkaloid wastewater effluent with membrane technology. In the experimental system, two parallel laboratory scale membrane bioreactors (MBR) with and without anaerobic pretreatment were used and the volume of each cylindrical MBR was 6 L with height and internal diameter of 35 cm and 14 cm, respectively (Fig. 1). MBR was established with microfiltration (MF) and ultrafiltration (UF) membrane modules at submerged mode in the bioreactor in series operation. Monitoring parameters were determined as pH, ORP (Oxidation Reduction Potential), temperature, and dissolved oxygen and were controlled with an online system. Before the treatment, the activated sludge was taken from the return sludge line at the leachate wastewater treatment plant and it was used for inoculation medium.

**Figure 1.** Laboratory scale MBR system

A flow chart of the membrane treatment scenarios is shown in Fig. 2. In the first scenario (Scenario-A) the raw wastewater (Fig 2a) was directly fed to the MBR system and the system was operated at different membrane types (MF and UF, named as Scenario-A1 and Scenario-A2). The MBRs were first operated at step-fed mode with gradually increasing ratios (raw wastewater volume/total volume) in order to acclimatize the biomass to opium alkaloid raw wastewater. After acclimation, the raw wastewater fed to parallel MBR-MF systems for Scenario-A1 and after reaching steady state conditions, UF modules were installed other MBR systems for Scenario-A2. Both MBR systems were tested at the same operating conditions. The effluent streams of MBR-MF and MBR-UF operations were simultaneously filtrated from NF and RO membranes at different recovery ratios for the polishing step. A 300-mL of stirred cell (Sterlitech HP4750, USA) was used for RO and NF filtration. The membrane diameter was 0.049 m and the effective membrane area was $1.46 \times 10^{-3} \text{ m}^2$. The maximum operating pressure for this cell was $69 \times 10^5 \text{ Pa}$.

In the second scenario (Scenario-B), the raw wastewater was first exposed to anaerobic pretreatment and then MBRs having MF and UF were used for second step biological treatment Scenario-B1 and Scenario-B2, respectively (as seen from Fig 2b). In the last scenario, (Scenario-B3) the anaerobic pretreated wastewater was directly filtrated from the UF membrane. For all the treatment strategies, similar to Scenario-A NF and RO membrane operations were used as a polishing treatment step.

Table 3. The properties of the anaerobic digester effluent

| Parameters | Value |
|---|--------------|
| pH | 8.2 |
| Soluble chemical oxygen demand (COD) (mg/L) | 2027±6 83 |
| Suspended Solid (SS) (mg/L) | 15900 |
| Color (PtCo) | 3887 |
| Particle size, µm | 0.032 |

At the anaerobic treatment phase, a laboratory scale anaerobic digester (W8) was used and the system consists two separate reactors (Armfield Ltd, UK). Anaerobic treatment experiments were carried out over a nine-month period. The details of this experiment were published by Çelen-Erdem et al. [16]. The effluent stream of reactor was fed to both MBR systems. The characteristics of the anaerobic digester effluent are shown in Table 3.

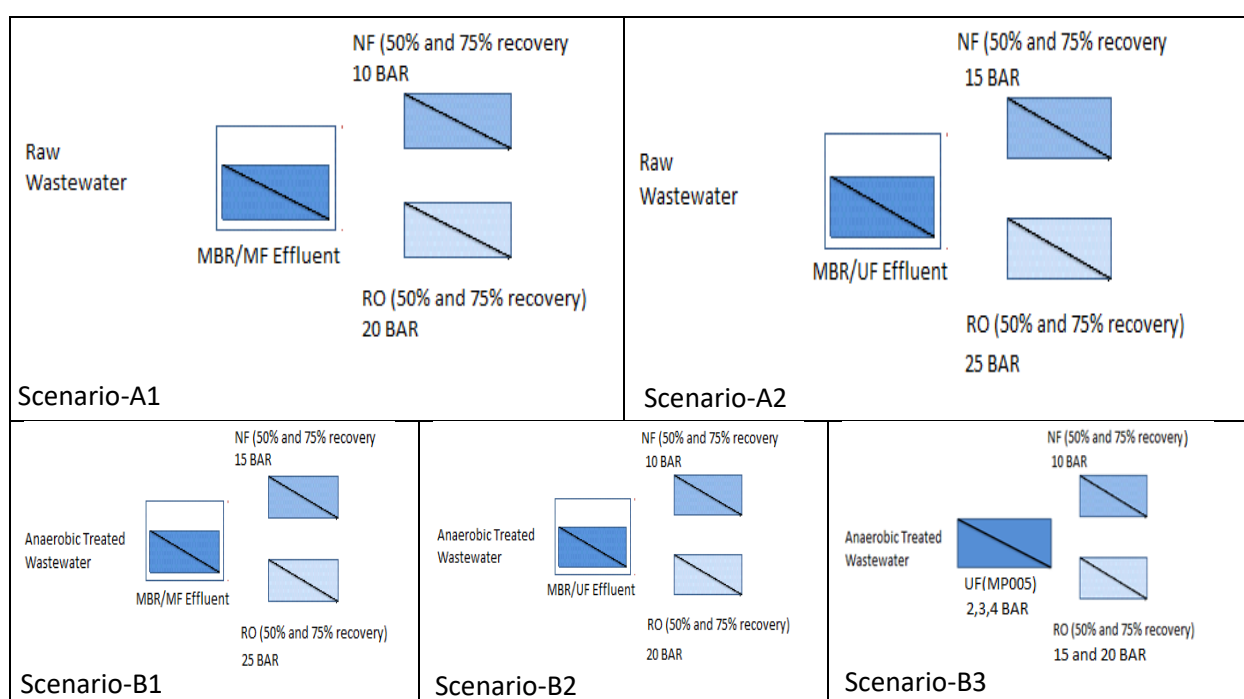


Figure 2. Membrane treatment strategies applied in experimental runs (a) Raw wastewater (b) Anaerobically pretreated wastewater

3. Results and Discussion

3.1. Treatability of raw alkaloid wastewaters with MBR operation (Scenario-A)

3.1.1. MBR operation

In this Scenario-A, the MBR system was fed gradually with raw opium alkaloid wastewater with step-fed mode to acclimatize the biomass. Two different membrane types were used for MBR operation as MF (Scenario-A1) and UF (Scenario-A2). The steady state conditions reached 60 days at MBR-MF and 80 days at MBR-UF, respectively.

The MLSS (Mixed Liquor Suspended Solids) concentration in the MBR reactor was measured at

around 15100 mg/L at the beginning of experiment. After the feeding of raw wastewater with step-fed mode, the MLSS and MLVSS (Mixed Liquor Volatile Suspended Solids) concentrations gradually increased in MBR and the trend is graphically shown in Figure 3a. The average values of MLSS and MLVSS concentrations were measured as 32555±16 mg/L, 40347±16 mg/L for MBR-MF and 25083±12 mg/L, 27164±11 mg/L for MBR-UF operations, respectively. The removal efficiency of organic

matter was evaluated by means of COD concentration removal. The average influent and effluent COD concentrations for MBR-MF were 15136 ± 89 mg/L and 1858 ± 96 mg/L, respectively. However, the average influent and effluent COD concentrations were 35713 ± 99 mg/L and 18529 ± 12 mg/L, respectively for MBR-UF. In this period, the most important operational drawback in MBR was the foaming problem during the experiment. For prevention of this problem, about 0.2-0.5 mL anti-foaming agent was used at everyday but it increased the effluent COD concentration and the COD removal efficiency was affected negatively [17,18]. As can be followed from the Figure 3b, the COD removal efficiencies for MBR-MF and MBR-UF were found as $86 \pm 9\%$ and $55 \pm 24\%$, respectively. Due to the very high load, the sieving effect on the particles improves the turbidity and suspended solids

in a very limited amount of suspended solids in the effluents from both MBRs [19,20].

As shown in Figure 3c, for MBR-MF the permeate flux value and daily treated wastewater flow were about 2 ± 0.9 L/m²h and 3.5 ± 1.6 L/day, respectively. However, when the MBR-UF was used the average the permeate flux value and daily treated wastewater flow were 2 ± 1.16 L/m²h and 3.5 ± 1.96 L/day, respectively. Color removal was not achieved as can be seen in Figure 3d. The approximate pH was 7.9 and ORP was 366 mV during the running time. At MBR operation with raw wastewater, it can be said that the flux and flowrate value of UF membrane were greater than that of MF membrane, although the COD values were increasing step by step. COD removal efficiencies of UF membrane were also higher than MF membrane.

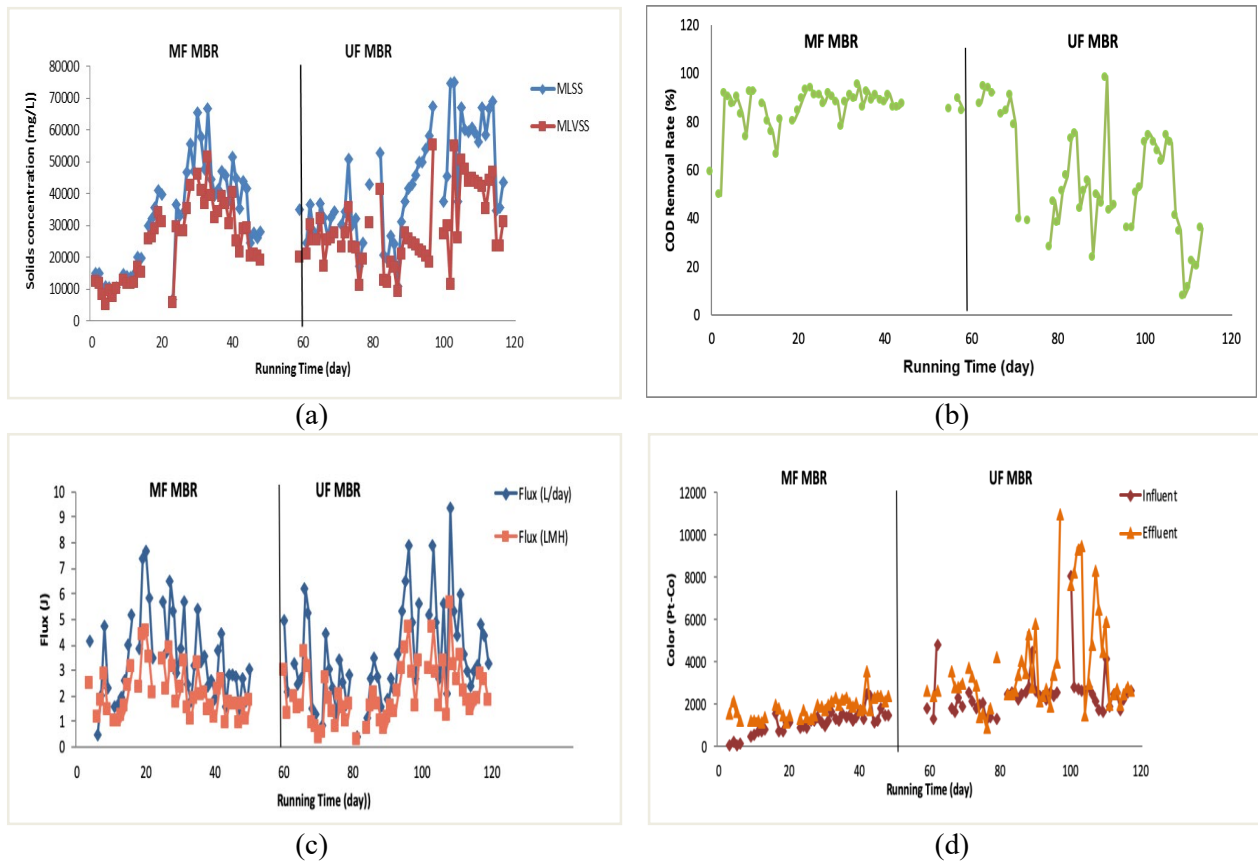


Figure 3. The graph of parameters during MBR operation with raw alkaloid wastewater (a) MLSS and MLVSS, (b) COD (c) Flux and (d) Color results

3.1.2. NF and RO treatment studies

In Scenario-A, the permeate streams from MBR/MF (scenario-A1) and MBR/UF (scenario-A2) were treated separately by NF (NF270 and NF90 membranes) and RO (XLE membrane) systems at two different recovery ratios (75% and 50%). The NF (NF 270 and NF 90) and RO (XLE) membranes were operated at two recovery ratios of 50% and 75%. RO experiments with raw wastewater indicated that the 99.6% COD and complete color removal was

achieved. The performance of RO membrane based on the removal efficiency of conductivity, COD, and color was higher than that of NF membrane (Table 4 and 5). In a study by Fazlioglu et al. [21] used industrial wastewater with MBR process and they investigated NF and RO membrane and their suitability for agricultural irrigation. They also found RO permeate more suitable for most of the parameters especially high conductivity removal efficiency.

Table 4. NF and RO experiment results of MBR-MF with raw alkaloid wastewater

| Membrane type | Pressure (bar) | Recovery Ratio (%) | Flux (LMH) | Conductivity (mS/cm) | | COD (mg/L) | | Color (Pt-Co) | |
|---------------|----------------|--------------------|------------|----------------------|----------|------------|----------|---------------|----------|
| | | | | Influent | Effluent | Influent | Effluent | Influent | Effluent |
| NF270 | 10 | 75% | 7.55 | 13.3 | 9.45 | 1220 | 300 | 3975 | 238.5 |
| NF270 | 10 | 50% | 10.8 | 13.3 | 8.72 | 1220 | 402.5 | 3975 | 148 |
| XLE | 15 | 50% | 6.45 | 13.3 | 1.5 | 1220 | 61.5 | 3975 | 119 |
| XLE | 15 | 75% | 2.6 | 13.3 | 1.8 | 1220 | 82.5 | 3975 | 108.5 |

Table 5. NF and RO experiment results of MBR-UF with raw alkaloid wastewater

| Membrane type | Pressure (bar) | Recovery Ratio (%) | Flux (LMH) | Conductivity (mS/cm) | | COD (mg/L) | | Color (Pt-Co) | |
|---------------|----------------|--------------------|------------|----------------------|----------|------------|----------|---------------|----------|
| | | | | Influent | Effluent | Influent | Effluent | Influent | Effluent |
| NF270 | 15 | 50% | 8.6 | 40.6 | 11.5 | 18500 | 9500 | 4625 | 498 |
| NF270 | 15 | 75% | 2.7 | 40.6 | 19.6 | 18500 | 1925 | 4625 | 461.5 |
| NF90 | 30 | 50% | 2.1 | 40.6 | 14 | 18500 | 1055 | 4625 | 629 |
| NF90 | 30 | 75% | 2.2 | 40.6 | 15.8 | 18500 | 1400 | 4625 | 1000 |
| XLE | 25 | 50% | 2.8 | 40.6 | 3.8 | 18500 | 244 | 4625 | 104.5 |
| XLE | 25 | 75% | 2.6 | 40.6 | 10.6 | 18500 | 322 | 4625 | 96 |

3.2. Treatment of anaerobically pretreated wastewater in MBR (Scenario-B)

3.2.1 MBR operation

In Scenario-B, the raw wastewater was firstly exposed to anaerobic treatment and then the effluent stream of anaerobic digester was fed to MBR-MF for 60 days and MBR-UF for 60 days. During the

experiments, two different membrane types were used for MBR operation of anaerobic treated effluent as MF (Scenario-B1) and UF (Scenario-B2). In Fig.4a, the change of MLSS concentration at MBR with anaerobic pretreated wastewater is given and the MLSS concentration was measured about 15900 mg/L at the beginning of the experiment. The average values of the MLSS become 10461 ± 52 mg/L and 16454 ± 76 mg/L in the MBR-MF and MBR-UF

reactors, respectively. The average values of MLSS and MLVSS concentrations were measured as 10461 ± 52 mg/L, 7326 ± 31 for MBR-MF and 16454 ± 76 , 7565 ± 27 mg/L for MBR-UF operations, respectively. The average influent and effluent COD concentrations for MBR-MF were 2120 ± 96 mg/L and 1401 ± 46 mg/L, respectively. However, the average influent and effluent COD concentrations for MBR-UF were 2847 ± 12 mg/L and 2466 ± 99 mg/L, respectively. As can be followed from the Figure 4b, the COD removal efficiencies for MBR-MF and MBR-UF were found as 41 ± 16 % and 24 ± 18 %, respectively.

As shown in Figure 4c, for MBR-MF the permeate flux value and daily treated wastewater flow were about 2.4 ± 0.9 L/m²h and 4 ± 1.7 L/day, respectively. However, when the MBR-UF was used the average the permeate flux value and daily treated wastewater flow were 3 ± 2.2 L/m²h and 5 ± 3.7 L/day, respectively. Color removal was not achieved as can be seen in Figure 4d. During the reactor performance HRT was approximately 1.25 days, pH and ORP were 9.0 and 366 mV respectively. Also, no sludge was discarded from the system.

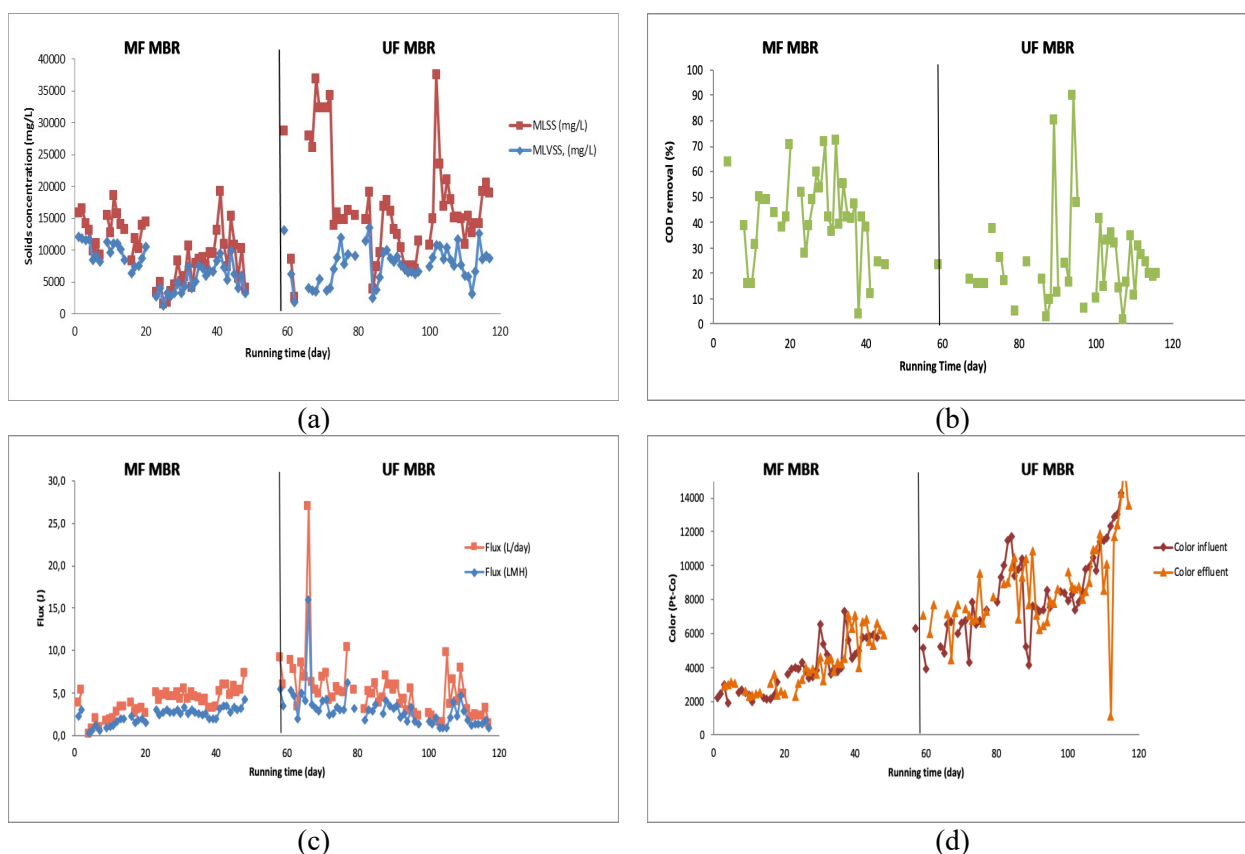


Figure 4. The graph of parameters during MBR operation with anaerobically pretreated alkaloid wastewater (a) MLSS and MLVSS, (b) COD (c) Flux, and (d) Color results.

3.2.2. NF and RO treatment studies

As shown in Figure 2b, two different types of membrane treatment strategies were applied to the anaerobically pretreated opium alkaloid wastewater. The effluents from MBR/MF (scenario-B1) and MBR/UF (scenario-B2) were treated by NF and RO units. Moreover, low COD removal of anaerobically pretreated opium alkaloid wastewater was determined in the MBR. Therefore, the NF and RO

membrane applications with UF pretreatment were used in order to increase the removal rates (Scenario-B3). The NF (NF 270) and the RO (XLE) membranes were operated at the recovery ratio of 50–75%. RO experiments with raw wastewater indicated that the 99.6% COD and complete color removal were achieved. The performance of RO membrane based on the removal efficiency of conductivity, COD, and color was higher than that of NF membrane (Table 6 and 7).

Table 6. NF and RO experiment results of MBR-MF with anaerobically pretreated alkaloid wastewater

| Membrane type | Pressure (bar) | Recovery Ratio (%) | Flux (LMH) | Conductivity (mS/cm) | | COD (mg/L) | | Color (Pt-Co) | |
|---------------|----------------|--------------------|------------|----------------------|----------|------------|----------|---------------|----------|
| | | | | Influent | Effluent | Influent | Effluent | Influent | Effluent |
| NF270 | 10 | 75 | 10.4 | 20.2 | 17.3 | 3700 | 1160 | 6925 | 369 |
| NF270 | 10 | 50 | 23.0 | 20.2 | 15.6 | 3700 | 120 | 6925 | 1010 |
| XLE | 20 | 50 | 3.4 | 20.2 | 7.1 | 3700 | 40 | 6925 | 149 |
| XLE | 20 | 75 | 3.2 | 20.2 | 14.9 | 3700 | 98 | 6925 | 170 |

Table 7. NF and RO experiment results of MBR-UF with anaerobically pretreated alkaloid wastewater

| Membrane type | Pressure (bar) | Recovery Ratio (%) | Flux (LMH) | Conductivity (mS/cm) | | COD (mg/L) | | Color (Pt-Co) | |
|---------------|----------------|--------------------|------------|----------------------|----------|------------|----------|---------------|----------|
| | | | | Influent | Effluent | Influent | Effluent | Influent | Effluent |
| UF-MP005 | 2 | 100 | 8.6 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| UF-MP005 | 3 | 100 | 8.6 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| UF-MP005 | 4 | 100 | 11.3 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| NF270 | 10 | 75 | 10.5 | 13.3 | 10.6 | 1680 | 306 | 2800 | 336 |
| NF270 | 10 | 50 | 14.7 | 13.3 | 9.5 | 1680 | 226 | 2800 | 364 |
| XLE | 15 | 50 | 2.9 | 13.3 | 2.9 | 1680 | 128 | 2800 | 107 |
| XLE | 20 | 75 | 3.5 | 13.3 | 2.0 | 1680 | 105 | 2800 | 84 |
| XLE | 20 | 50 | 10.4 | 13.3 | 1.0 | 1680 | 51 | 2800 | 70 |

Table 8. NF and RO experiment results of UF with anaerobically pretreated alkaloid wastewater

| Membrane type | Pressure (bar) | Recovery Ratio (%) | Flux (LMH) | Conductivity (mS/cm) | | COD (mg/L) | | Color (Pt-Co) | |
|---------------|----------------|--------------------|------------|----------------------|----------|------------|----------|---------------|----------|
| | | | | Influent | Effluent | Influent | Effluent | Influent | Effluent |
| | 2 | 100 | 8.6 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| UF-MP005 | 3 | 100 | 8.8 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| | 4 | 100 | 11.3 | 13.5 | 13.3 | 3140 | 1680 | 5280 | 2800 |
| NF270 | 10 | 75 | 10.5 | 13.3 | 10.6 | 1680 | 306 | 2800 | 336 |
| NF270 | 10 | 50 | 14.7 | 13.3 | 9.5 | 1680 | 226 | 2800 | 364 |
| XLE | 15 | 50 | 2.9 | 13.3 | 2.9 | 1680 | 128 | 2800 | 107 |
| XLE | 20 | 75 | 3.5 | 13.3 | 2.0 | 1680 | 105 | 2800 | 84 |
| XLE | 20 | 50 | 10.4 | 13.3 | 1.0 | 1680 | 51 | 2800 | 70 |

At the last part of the experiments, UF-MP005 was applied to the effluents of anaerobically treated opium alkaloid processing effluent as pretreatment (Figure 2b). Experimental results indicated that COD, color, and conductivity removals of 46%, 47%, and 0%, respectively, were possible at a pressure of 2, 3, 4 bar as shown in Table 8. The NF (NF 270) and reverse osmosis were applied to the UF pretreated effluent. It demonstrated that the pretreatment before NF and XLE is necessary to obtain high conductivity, COD and color removal.

COD removal of anaerobically pretreated opium alkaloid wastewater was very low in the MBR treatment experiments. However, when NF membrane application with UF pretreatment option was applied, 82% COD and 88% color removal were obtained at 75% recovery. The removal efficiencies

of COD and color were as 94% and 97%, respectively, were achieved for NF runs with UF pretreatment.

3.3 Performance evaluation of all scenarios

To describe results of experiments, performance of all scenarios was compared in terms of flux, COD and conductivity rejections. As shown in Table 9, permeate values for COD, color and conductivity did not change significantly for the XLE-RO membrane with 75% recovery ratio. However, anaerobic pretreatment strongly influenced the solute rejections by NF and RO, probably due to lower contact time to solutes with membrane surface because the flux was nearly doubled than raw waste water system. It was seen that although most of the parameters make RO permeate more suitable than NF except flux.

Table 9. Comparison of permeate qualities all scenarios.

| Type | Parameter | Units | Permeates | | | | |
|--|--------------|-------|--------------------|--------|--------|--------------------|-------|
| | | | 50% Recovery Ratio | | | 75% Recovery Ratio | |
| | | | XLE | | | NF 270 | XLE |
| | | | NF 270 | 15 bar | 20 bar | NF 270 | XLE |
| Raw Waste Water + MBR MF (Scenario-A1) | Flux | LMH | 10.8 | 6.45 | | 7.55 | 2.6 |
| | COD | mg/L | 402.5 | 61.5 | | 300 | 82.5 |
| | Color | Pt-Co | 148 | 119 | | 238,5 | 108,5 |
| | Conductivity | mS/cm | 8.72 | 1.5 | | 9.45 | 1.8 |
| Raw Waste Water + MBR UF (Scenario- A2) | Flux | LMH | 8.6 | | 2.8 | 2.7 | 2.6 |
| | COD | mg/L | 9500 | | 244 | 1925 | 322 |
| | Color | Pt-Co | 498 | | 104,5 | 461.5 | 96 |
| | Conductivity | mS/cm | 11.5 | | 3.8 | 19.6 | 10.6 |
| Anaerobically Pretreated Wastewater + MBR MF (Scenario-B1) | Flux | LMH | 23 | | 3.4 | 10.4 | 3.2 |
| | COD | mg/L | 120 | | 40 | 1160 | 98 |
| | Color | Pt-Co | 1010 | | 149 | 369 | 170 |
| | Conductivity | mS/cm | 15.6 | | 7.1 | 17.3 | 14.9 |
| Anaerobically Pretreated Wastewater + MBR UF (Scenario-B2) | Flux | LMH | 14.7 | 2.9 | 3.5 | 10.5 | 3.5 |
| | COD | mg/L | 226 | 128 | 51 | 306 | 105 |
| | Color | Pt-Co | 364 | 107 | 70 | 336 | 84 |
| | Conductivity | mS/cm | 9.5 | 2.9 | 1 | 10.6 | 2 |
| Anaerobically Pretreated Wastewater + UF (Scenario-B3) | Flux | LMH | 14.7 | 2.9 | 10.4 | 10.5 | 3.5 |
| | COD | mg/L | 226 | 128 | 51 | 206 | 105 |
| | Color | Pt-Co | 364 | 107 | 70 | 336 | 84 |
| | Conductivity | mS/cm | 9.5 | 2.9 | 1 | 10.6 | 2 |

4. Results and Discussion

In this study, the treatment of opium alkaloid wastewater was studied with 5 different scenarios. There is a limited number of studies investigating treatment of opium alkaloid wastewater in the literature. Table 10 summarizes the key performance parameters reported in the literature([12] and [22]) for different operations. The usage of NF membrane with MBR system enhanced the NF performance.

The results can be summarized as follows.

(1) The high COD concentration of the wastewater in the MBR experiments caused severe problems such as foaming problem, the chemical usage to prevent foaming. In order to prevent those problems, the wastewater was anaerobically pretreated.

(2) 99.6% COD and complete color removal were achieved with the RO experiments with alkaloid wastewater.

(3) Very low COD removal of anaerobically pretreated opium alkaloid wastewater was obtained in the MBR treatment experiments. The best treatment scenario for the anaerobically pretreated opium alkaloid wastewater was using RO unit following MBR/UF.

(4) COD removal of concentrated opium alkaloid wastewater was 46% in the MBR system. However, when the NF and RO membrane applications were applied, the COD removals were increased to 94% and 99.6%, respectively.

(5) For both concentrated and anaerobically pretreated opium alkaloid wastewater treatment scenarios, permeate flux value was increased with NF application.

Table 10. Comparison of the treatment performance of Opium Alkaloid Wastewater with this study.

| Pretreatment | Membrane Systems | Advanced Treatment | Operation Parameter | Flux (LMH) | COD Removal (%) | Conductivity Removal (%) | Color Removal (%) | Scale | References |
|--|------------------|--------------------|---------------------|------------|-----------------|--------------------------|-------------------|------------|------------|
| Anaerobic Treatment | MBR MF | NF 270 | 10 bar, % 50 RR | 23 | 97 | 23 | 85.4 | Laboratory | This study |
| | | RO (XLE) | 20 bar, % 50 RR | 3.4 | >98 | 65 | 97.5 | Laboratory | |
| | MBR UF | NF 270 | 10 bar, % 50 RR | 14.7 | 86.5 | 28.Haz | 87 | Laboratory | |
| | | RO (XLE) | 20 bar, % 50 RR | 10.4 | 97 | 92.4 | 97.5 | Laboratory | |
| - | UF | RO (XLE) | 20 bar, % 50 RR | 10.4 | 97 | 92.5 | 97.5 | Laboratory | |
| | MBR MF | NF 270 | 10 bar, % 50 RR | 10.8 | 67 | 34 | 96 | Laboratory | |
| | | RO (XLE) | 15 bar, %50 RR | 6.45 | 93 | 95 | 97 | Laboratory | |
| 2-stage Aerobic Treatment | MBR UF | RO (XLE) | 25 bar, % 50 RR | 2.8 | >98 | 90.6 | 97.7 | Laboratory | |
| | | NF 90 + NF 270 | 30 bar, %75 RR | 15 | 95 | 88 | >98 | Pilot | |
| 2-stage Aerobic Treatment | UF | NF | 24 bar, % 70 RR | 70 | >97 | 94 | >99 | Laboratory | |
| | | NF | 18 bar, % 70 RR | 12 | 97 | >98 | >99 | Pilot | |
| 2-stage Aerobic Treatment + Anaerobic Treatment Anaerobic Pretreated | UF | RO | 25 bar | 16 | 98 | 99 | >99 | Laboratory | |
| | | NF | 24 bar | 33 | 95 | 88 | >98 | Laboratory | [22] |

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Conflicts of Interest

The authors state that did not have conflict of interests

Abbreviations

| | | | |
|------|---------------------------------|-------|--|
| AIC | Anaerobic Internal Cycling | MLVSS | Mixed Liquor Volatile Suspended Solids |
| BOD | Biological Oxygen Demand | NF | Nanofiltration |
| COD | Chemical Oxygen Demand | OLRs | Organic Loading Rates |
| EC | Electrodialysis | ORP | Oxidation Reduction Potential |
| HRTs | Hydraulic Retention Times | RO | Reverse Osmosis |
| IWA | International Water Association | UASB | Upflow Anaerobic Sludge Bed) |
| MBR | Membrane Bioreactor | UF | Ultrafiltration |
| MF | Microfiltration | VFA | Volatile Fatty Acids |
| MLSS | Mixed Liquor Suspended Solids | WAO | Wet Air Oxidation |

Conflicts of Interest

The authors state that did not have conflict of interests.

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